

井工厂井网部署与压裂模式发展现状与展望

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摘要: 随着我国油气对外依存度逐渐加剧, 致密油气、页岩油气等非常规油气能源成为了我国能源发展的重点方向。井工厂压裂技术因其可以改造低渗透性地层、大幅降低施工成本、缩短施工周期、提高设备利用率、节约用地而被广泛应用于非常规油气开发之中。本文在论述井工厂压裂技术发展现状的基础上, 介绍了丛式水平井的井筒走向、水平段长度、井筒间距等井网部署特点, 统计分析了水平井分段分簇的裂缝长度、簇间距和射孔簇数等关键技术参数特点; 介绍了丛式水平井井工厂压裂常用的压裂方式, 包括双井同步压裂、双井拉链式压裂和多井组合压裂等, 对比分析了各种压裂方式的利弊。建议有针对性的发展立体井网井间裂缝干扰预测、井丛压裂孔簇设计等理论, 为我国非常规油气储层井工厂压裂技术发展指明了方向。

关键词: 水力压裂; 井工厂压裂; 丛式水平井; 分段分簇; 井网部署; 井丛压裂; 立体井网; 非常规油气

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Development status and prospect of well pattern deployment and fracturing mode in well factory

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Abstract: With the increasing dependence on foreign oil and gas, unconventional oil and gas energy such as tight oil and gas and shale oil and gas have become the focus of China's energy development. Well factory fracturing technology is widely used in unconventional oil and gas development because it can reconstruct low-permeability formations, significantly reduce construction costs, shorten construction time, improve equipment and land utilization. Based on the discussion of the development status of well factory fracturing technology, this paper introduces the well pattern deployment characteristics of cluster horizontal wells, such as wellbore direction, length of horizontal sections, wellbore spacing and further statistically analyzes the key technical parameters of horizontal wells in segmented clusters, such as fracture length, cluster spacing and perforating cluster number. Moreover, the fracturing methods commonly used in cluster horizontal well factory fracturing are also introduced, including dual-wells simultaneous fracturing, dual-well zipper fracturing and multi-well combination fracturing, and the advantages and disadvantages of the common fracturing methods are analyzed by contrast. It is suggested that the theories such as prediction of interwell fracture interference and well cluster fracturing perforation cluster design should be developed. The research points out the direction for the development of well fracturing technologies for unconventional oil and gas reservoir in China.

Key words: hydraulic fracturing; well factory fracturing; cluster horizontal well; segment clustering; well pattern deployment; cluster fracturing; three-dimensional well pattern; unconventional oil and gas

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0 引言

致密油气、页岩油气储层通常具有低孔低渗特点,水平钻井和水力压裂技术是开发此类储层的两大核心技术。随着水力压裂技术在非常规油气储层的大规模应用,当位于一个区块的多口井需要压裂时,每口井分别进行压裂设备搬迁、安装和压裂液配备,不但会延长工期也会增加生产成本。加拿大能源公司最先提出了井工厂水力压裂技术,并被用于北美页岩气开发,目前已经形成了一套较为成熟的开发模式^[1-2]。

中国也广泛地采用井工厂压裂技术,长宁地区龙马溪组页岩气采用拉链式压裂改造模式,完成2个水平井组7口井的压裂实践,较单独压裂作业效率提高1倍^[3]。川南地区五峰组—龙马溪组页岩气地区受地形限制,采用整体化的工厂压裂技术,使得钻井、压裂作业效率提高50%以上,设备安装时间减少70%,6口井的平台建设周期降至约1年^[4]。焦石坝页岩气田,采用小型丛式井工厂压裂技术,在40多个平台200余口井完成4000余段压裂,平均单井无阻流量为 $38.5 \times 10^4 \text{ m}^3/\text{d}$,相比单井施工周期缩短30%~40%^[5]。东辛油田盐227块致密砂砾岩油藏累计实施Y227、L567等8个井工厂整体压裂,在实现高效开发的前提下累计节约投资4.3亿元^[6]。

与传统的单井压裂作业相比,井工厂压裂技术优化了施工模式和顺序,一方面其提高了设备利用率,减少了搬迁与安装时间;另一方面,方便回收和处理井下压裂液^[7],既能充分利用水资源,又降低了环境污染风险。

近些年,井工厂压裂技术得到了较大的发展,包括:丛式水平井井网布置、段簇优化设计、多级压裂、同步压裂、拉链压裂、多井组合压裂等。笔者对井工厂压裂技术的特点和现状进行了分析,并阐述了相关技术的应用情况,以期促进中国井工厂压裂技术的发展。

1 丛式水平井井网部署与段簇设计

1.1 丛式水平井井网部署

丛式水平井井网部署(图1)是页岩油气开发中重要的环节,其主要受油气田地质特点、井群产能和总体经济效益控制。主要涉及:水平井数量、井筒走向、水平段长度、井筒水平间距和垂向间

距等。

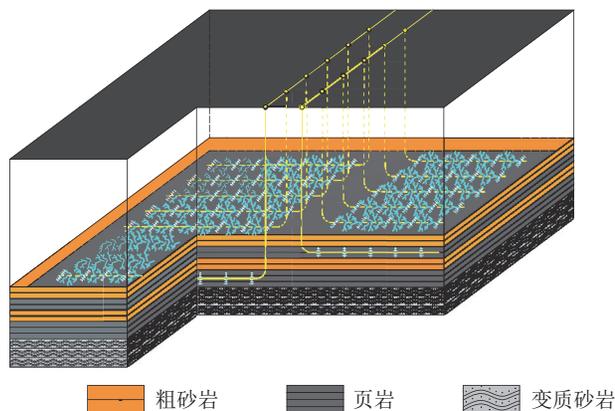


图1 井工厂井网空间布置^[8]

Fig.1 Space layout of well pattern in well factory

1.1.1 水平井井筒走向

水力裂缝一般会垂直于最小水平主地应力方向延伸,但由于钻井技术和工程地质条件限制,水平井往往会与最小水平主应力方向成一定角度(见表1),致使井筒与之产生的水力裂缝不完全垂直。水平井横切裂缝与纵向裂缝相比,可以避免裂缝重叠和段间连通的可能性,最大限度的扩大储层接触面积。随着裂缝与井筒夹角的增大,裂缝间距变大,缝间渗流干扰作用降低,油气产量有增加的趋势^[9]。因此,在钻井技术和储层地应力条件允许的情况下,井筒应与最小水平主应力平行或小角度相交,有利于形成垂直于井筒的多条横切裂缝,实现用一口水平井代替多口直井的目的。

1.1.2 水平井水平段长度

长水平段水平井是以大限度暴露储层为目的,通过增加储层与井筒的接触达到高产的一种井型。对于非裂缝性油藏,水平井产能可高达直井的3倍;对于裂缝性油藏,水平井产能可高达直井的12倍;对于超低渗油藏,长水平段的水平井也可以大幅度提高油气采收率。2018年,北美的水平段长度极限达到6340 m^[16],Range资源公司已经有78%的水平井水平段长度>2438 m。2021年,川庆钻探刷新中国超长水平井记录,水平段长度达到5256 m,中国涪陵页岩气井平均水平段长2078 m。

水平井需要根据矿场情况、油藏特征、经济性的因素,选取合理长度^[17]。当水平段长度>2000 m后,钻井作业效率会快速下降^[18],故目前大量油气

表1 水平井井筒走向

Table 1 Wellbore direction in horizontal wells

区块	储层岩性	最小水平地应力方向/(°)	井筒方位/(°)	最小水平地应力与水平段角度/(°)
苏53气田区块 ^[10]	石英砂岩	330~350	347	-3~17
塔里木哈拉哈塘油田区块 ^[11]	缝洞型碳酸盐岩	10~20	16.52	-3.48~6.52
大牛地气田DP4井 ^[12-13]	岩屑石英砂岩	165	156	-9
吉林油田长平3井 ^[14]	致密砂岩	267	260	-7
鄂尔多斯盆地庆城油田H100平台 ^[15]	细砂岩、粉砂岩、页岩	340~350	339.25	-0.75~10.75

田将水平段长度设定在1000~2000 m之间(见表2)。同时水平井水平段长度也呈现出增加的趋势,单个井平台的可动用储层范围逐渐增大。

表2 水平井水平段长度

Table 2 Length of horizontal section in horizontal wells

区块	储层岩性	开钻年份	水平段长度/m
苏里格气田 ^[10, 19]	石英砂岩	2010	805~1256
大牛地气田盒1层 ^[20-21]	岩屑石英砂岩	2012	1239.5(平均)
加拿大Duvernay页岩油田 ^[22]	海相页岩、泥质灰岩	2012—2018	1300→3000
Range公司二叠系盆地 ^[23]	—	2012—2018	951.89→3088.54
Haynesville页岩气田 ^[24-25]	碳酸盐、泥岩	2009—2016	1350→2155
威204页岩气井区 ^[26]	深水陆棚、钙质浅水陆棚页岩	2016—2020	1506→1965
鄂尔多斯盆地庆城油田H100平台	细砂岩、粉砂岩、页岩	2021	1900~3000

注:→表示在年份区间内水平段长度变化。

1.1.3 水平井井筒间距

井工厂裂缝扩展与干扰规律是水平井压裂的难题,目前裂缝干扰研究主要集中在裂缝间影响,关于井间距对裂缝扩展干扰研究不足。井间距是控制储层改造效果和优化井产能的关键,应在合理井间干扰范围内降低井工厂井间距^[27]。当丛式水平井井筒间距较大时部分储层不能动用,过小则存在由于井的覆盖面积重叠导致井间渗流干扰、应力干扰以及单井的经济效益下降的风险。砂体规模尺度、压降泄气范围、干扰试井、水力裂缝半长是确定井间距的重要依据^[28]。当储层较厚或者具有多个含油层系的情况下,采用多层布井、立体交错布井的“W”形立体布井方式,在横、纵向上选择合适的井间距,达到立体开发储层的目的。涪陵页岩气采用多层系精细开发,横向加密加长、纵向上多层系扩展,形成立体空间密织井网,有效提高储层动用率。中国每个生产平台通常布置6~8口水平井,北美成熟的井工厂平台一般可以钻16~20口井^[29](见表3),大平台、大井丛已经成为了一种开发

趋势。

1.2 水平井分段分簇

页岩油气、致密油气储层的水平井水平段一般

表3 水平井井筒间距

Table 3 Horizontal wellbore spacing

区块	储层岩性	井间距/m	平台井数/口
中国蜀南地区 ^[30-32]	深水陆棚页岩	400~500	—
涪陵页岩气地区 ^[33]	深水陆棚页岩	300~740	7~8
长宁-威远页岩气区块PT2平台 ^[34]	深水陆棚、钙质浅水陆棚页岩	200~400	6
准噶尔盆地昌吉油田 ^[35]	泥岩、砂砾岩	310~350	7~12
鄂尔多斯盆地庆城油田H100平台	细砂岩、粉砂岩、页岩	175~350	31
Utica页岩气田 ^[36]	陆表海页岩	259~366	—
Bakken页岩气田 ^[37]	黑色泥页岩	302~402	8~17
Eagle Ford页岩气 ^[38]	泥灰岩、灰质页岩	60~150	—
北美页岩气田(平均) ^[39]	—	180~420	16~20

长达数千米,储层改造时需将水平段划分为多个井段,每个井段含有多个射孔簇,形成了水平井多段多簇压裂改造技术。

1.2.1 裂缝长度

日产量通常随着水力裂缝长度的增加而增高,但是增加的幅度不断下降,因此存在最佳裂缝长度,其受到压裂方法、地应力分布、水平井分布的影响,在最佳裂缝长度后增产效果和压裂投入不成正比^[40]。

对于单口水平井压裂,当裂缝半长沿水平井分布为两端长中间短情况时(见图2),类似于U形布缝方式,外侧的裂缝对于总产量的贡献大于内侧裂缝的贡献^[41],更好的扩大了流体椭圆渗流区域,降低了流体渗流阻力^[42]。

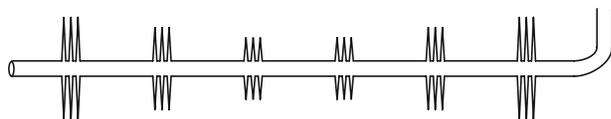


图2 裂缝长度沿井筒分布规律

Fig.2 Distribution law of fracture length along wellbore

对于单个压裂段而言,U形布缝外侧裂缝较长,控制范围较大,中间裂缝对于产量影响较少。数值模拟表明,U形布缝累计产能>反U形布缝累计产能>锯齿形布缝累计产能(见图3)^[43]。

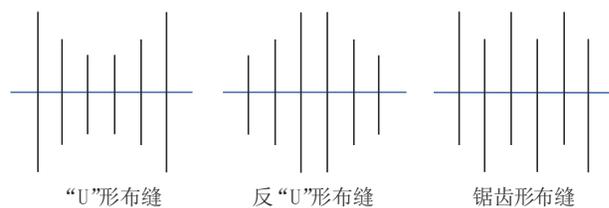


图3 布缝方式

Fig.3 Fracture arrangement

对于多井压裂,在设计井间距与裂缝长度时应考虑压裂过程中井间裂缝互相干扰的影响,使得相邻井裂缝内部的压裂液互相沟通而支撑剂未沟通的程度,有效利用井间应力干扰使裂缝复杂化^[44]。裂缝长度可以出于强化平面有利干扰原则,按照井距的2/3~3/4设计裂缝半长,实现缝长交叉,避免超长缝长引起的不利干扰^[44]。庆城县南庄乡西233井区水平井优化裂缝半长为80~180 m。滨425区块^[45]以3年累计产油量优化裂缝半长为70~90 m。

陈汾君等^[46]对新场气田沙二气藏中四口井进行产能优化,指出其最优裂缝长度为70~110 m。

国内外对于裂缝间距与缝长设计时,大多采用等间距和缝长,且在产能预测的时候进行一定简化与近似,考虑井间干扰与缝间干扰较少,与现场的实际情况存在一定差距。

1.2.2 簇间距

簇间距对油气产能影响较大,通常随着簇间距增大,井间干扰减小,单裂缝产量增高,但是总体经济效益较低。裂缝间距越小,缝间应力干扰严重,但储层沟通更为充分,初期产能较高^[47-48],后期产量递减较快。由于地层厚度、天然裂缝、地应力、脆性指数等的非均匀性,往往会导致地质甜点和工程甜点区域不连续。现场压裂实践认为,在甜点区射孔压裂会最大程度实现裂缝开启和缝网改造^[49],因此,在布置簇间距时应尽量避免缝间应力干扰产生的副作用,又能沟通甜点区域^[50]。

当采用非均匀簇间距设计时,不同的裂缝间距组合对水平井产量影响很大。采用两侧裂缝间距较小,而井筒中部裂缝间距较大的时候,产能明显优于其他情况,这是因为水平井两端裂缝渗流控制区域大于井中间段的控制区域(见图4)。



图4 簇间距沿井筒分布规律

Fig.4 Distribution law of cluster spacing along wellbore

裂缝间距设计一般基于整体经济效益评价、产能模拟最大化的结果^[51],同样也需要考虑主应力差、可压性等因素的影响。当水平最大与最小主应力较接近,尤其是水平应力非均质系数 <0.2 时较易形成复杂裂缝^[52]。因此,确定裂缝间距时需要考虑诱导应力和裂缝距离的关系,使得诱导应力可以大于裂缝张开的压力^[53-54]。

表4可以看出目前射孔簇间距在合理范围内呈现缩短的趋势,缩短簇间距可以让簇间应力干扰增强,裂缝转向和裂缝复杂度得到提高,簇间储层得到更充分利用。

1.2.3 射孔簇数

在使用水力压裂技术改造油气储层的过程中,通常在一个水平压裂段中使用多个射孔簇去降低

表 4 水平井簇间距

Table 4 Horizontal cluster spacing

区块	年份	簇间距/m
Midland Basin ^[55]	2010—2017	16.7→7.6
长宁页岩气 ^[56]	2014—2019	27→16
鄂尔多斯盆地庆城油田 H100 平台	2021	8~20
Eagle Ford ^[57]	2014—2017	16.7→4
威页 X-4HF 页岩气井 ^[58]	2020	8.4~9.9
Permian Basin ^[59-60]	—	16→4.5

注:→表示在年份区间内簇间距变化。

单口井的总压裂段数。但是由于 1/3 的压裂簇无效,因此,应合理的设计簇数与单个段长。

在簇间距一致的条件下,簇数越多产生的无效裂缝越多,产量越低;需要在单段内尽量选岩性及力学性质相似的井段布置射孔簇。射孔簇位置应以地质甜点为前提,优选段内岩性、物性、脆性、地应力差异性较小的区域,尽量选择天然裂缝发育的区域,避免对产层、非产层段同时射孔。在压裂实践中,应由简单的追求压裂波及体积转变为在有限的波及内尽可能提高体积裂缝密度,由井控储量模式转变为缝控储量模式,增加产能^[61]。

表 5 列举了一些典型页岩油气区块的单段长度和簇数,目前在储层改造过程中形成了单段簇数增多,簇间距缩短的加密切割发展趋势。

表 5 水平井分段段长与单段簇数

Table 5 Section length and cluster number of single segment in horizontal wells

区块	储层岩性	分段段长/m	单段簇数
Permian Basin 页岩气区块 ^[59]	硅质页岩	90~108→ 30~35	平均 3→ 平均 10
Bakken 页岩气区块 ^[62]	黑色泥页岩	70~105	6~15
加拿大 Duvernay 页岩气田 ^[63-64]	海相页岩、泥质灰岩	平均 90→ 均 49	6~7
长宁-威远国家级页岩气 ^[65]	深水、浅水陆棚页岩	17.49~50.26	—
吉木萨尔页岩油 ^[66-67]	灰色泥岩、夹砂质泥岩	60~90	5~12
鄂尔多斯盆地庆城油田	细砂岩、粉砂岩、页岩	15~50	3~5

注:→表示该区块变化趋势。

2 井工厂水力压裂常用的压裂方式

井工厂常见的压裂方式为双井同步压裂、双井拉链式压裂和多井组合压裂等。

2.1 双井同步压裂技术

同步压裂技术(见图 5)即在压裂过程中,同时对两个及以上平行的相邻井进行压裂,压裂液和支撑剂在两口井之间的运移距离最短,从而使得不同的井之间产生沟通效果,大大提高了裂缝的导流能力,同时可以增加水力裂缝网络密度和增加压裂作业时产生的表面积,产生更加复杂的三维裂缝网络^[68]。目前同步压裂技术不只限于 2 口深度相似且距离接近的井,已经可以满足 3~4 口水平井同时压裂^[69]。

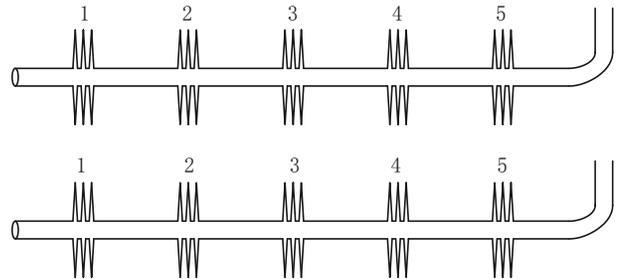


图 5 双井同步压裂(压裂顺序如图中 1→5)

Fig.5 Dual-well simultaneous fracturing (fracturing sequence as 1→5)

同步压裂技术在美国 Barnett 页岩气井开发得到了广泛应用,显著提高了页岩气井的产能^[66]。俄克拉荷马州东部的 Woodford 页岩地区采用了同步水力压裂开发策略,盆地西部地区的初始产量增加了 20%,东部地区增加了 72%^[70]。美国得克萨斯州沃斯堡盆地公布的数据显示,在相邻的两口页岩气水平井中采用同步压裂技术,产量得到显著提高。苏 53 区块致密砂岩气田采用工厂化同步压裂储层改造措施,优选 6 口水平井实施双井同步压裂,单井日产气量 $11.80 \times 10^4 \text{ m}^3/\text{d}$,比苏 53 区块 13 年投产水平井产气量高 $0.49 \times 10^4 \text{ m}^3/\text{d}$ ^[71]。

2.2 双井拉链式压裂技术

双井拉链式压裂即在多井平台上一口井进行压裂作业,一口井进行电缆桥塞射孔作业,两口井交替压裂,同时在另外一口井中下入裂缝监测设备实时监测裂缝参数,可以降低非生产时间。详细作业即对于 1、2 两口井进行拉链压裂作业,电缆等设备在 1、2 井中交替使用同时完成下桥塞和坐封作

业,在压裂其他井时1、2井进行钻磨桥塞等其他作业,而后在都完成钻磨桥塞等作业后统一放喷排液。拉链压裂产生的微地震事件明显多于单井压裂产生的微地震事件,丛式井平台拉链式压裂可以大幅度改造储层达到增产的目的,同时采用拉链式压裂井间的应力干扰有利于裂缝发生转向生成更好的裂缝网络^[72]。

2.2.1 传统拉链式压裂

传统的双井拉链式压裂(见图6)即将两口水平井射孔簇安放在相同位置,使得各个裂缝相对生成,可以最大限度的提高每个裂缝尖端的应力扰动,但是该扰动仅限于裂缝尖端区域^[73]。

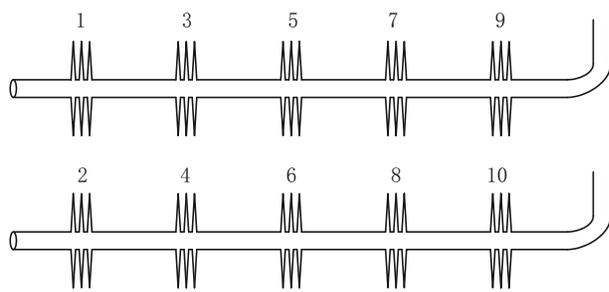


图6 双井拉链压裂(压裂顺序如图中1→10)

Fig.6 Dual-well zipper fracturing (fracturing sequence as 1→10)

2.2.2 改进拉链压裂

传统拉链式压裂虽然可以减小水平应力各向异性,但是实际操作过于复杂,改进的拉链式压裂(见图7)将拉链式压裂与交替压裂结合,将裂缝设计为交错模式,使得形成更多的复杂裂缝^[74-75]。改进拉链压裂中诱导应力对裂缝扩展影响较小,裂缝宽度分布较均匀,同时其可以产生较大的诱导应力,但是主应力方向变化较小,最佳裂缝间距小于顺序压裂与交替压裂^[76]。

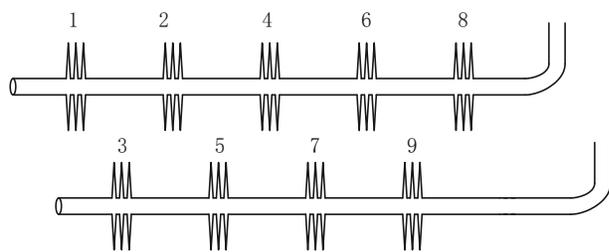


图7 改进的双井拉链压裂(压裂顺序如图中1→9)

Fig.7 Improved dual-well zipper fracturing (fracturing sequence as 1→9)

2013年,中国石油首次应用拉链式压裂技术对长宁平台进行页岩气工厂化压裂,平均每天压裂3.16段,极大地提高了压裂时效^[77]。涪陵页岩气田井工厂技术设计双井拉链压裂与双机组同步压裂方式,较好的完成了建平台、钻井、压裂、产气的开发要求。威远W202H2区块采用多井拉链作业,在444 d内完成103级(299簇)压裂,注入流体189023 m³与支撑剂6677 m³,节约成本约600万美元^[78]。焦石坝区块目前已经完成了40多个多井平台、200口井、4000级改进式拉链压裂工作,单井平均产出流量38.5×10⁴ m³/d,工期缩短30%~40%,单井产能和施工效率明显提高^[79]。美国Eagle Ford采用拉链压裂方式使初始产量提高了20%~40%^[80]。墨西哥北部盆地运用改进式拉链水力压裂技术,经过32级水力压裂后,单口水平井初始产量为4160桶/天,初始产量达到常规井的15倍以上,90 d累计产量为常规产量的14倍以上^[81]。

2.3 多井组合压裂

在多井压裂中,如果两口井产生的应力正面相交则可能导致应力抵消,减缓裂缝的延伸,而当斜向相交情况下,可以通过剪切形成新的裂缝,促进压裂的效果^[82]。因此可以通过不同的压裂顺序,利用缝间应力干扰,提高压裂效果。

在多井组合压裂中拉链压裂较为流行,即一口井进行泵送,另外一口井进行电缆作业,减少了压裂过程中的停机时间,提高了作业效率。通常情况下,一次压裂作业的井不超过4口,单层3口井拉链压裂按照是否考虑中间井筒的延后可以分为两种^[83-84](见图8、图9)。

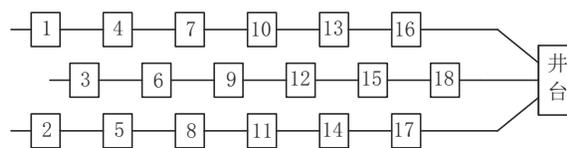


图8 单层3口井拉链压裂

Fig.8 Zipper fracturing of three wells in single formation

单层4口井拉链压裂按照相邻井分组和间隔井分组可分为两种^[83-84]:第一种是将4口井分为两组,1、3两口井先进行拉链压裂,而后2、4两口井再进行拉链压裂(见图10);另外一种是可以将两口井拉链压裂扩展到多井压裂,压裂作业从井场边缘由外向内,优先两侧井压裂可以减少中间区域的水平应力

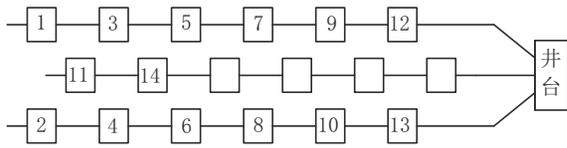


图 9 单层 3 口井拉链压裂(中间井筒延后)

Fig.9 Zipper fracturing of three wells in single formation (with intermediate shaft lag)

差,为形成复杂裂缝和降低断层滑动风险提供条件(见图 11)。

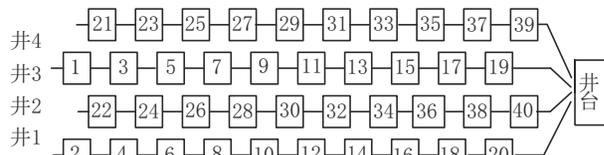


图 10 单层 4 口井拉链压裂(间隔井为一组)

Fig.10 Zipper fracturing of four wells in single formation (spaced wells are grouped)

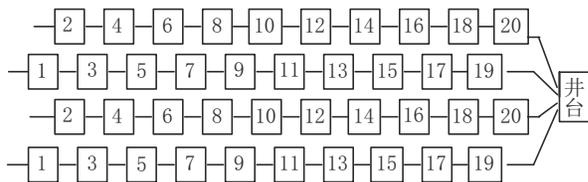


图 11 单层 4 口井拉链压裂(相邻井为一组、且从井场边缘向内压裂)

Fig.11 Zipper fracturing of four wells in single formation (adjacent wells are grouped together and fractured inwards from the edge of the well site)

常规的 3、4 口井的拉链压裂方式更容易使得产生的水力裂缝向着天然存在的薄弱面靠近,增加了裂缝之间的干扰程度,限制了新的裂缝的产生数量,而中间井筒延后和由边缘向内压裂的拉链压裂方式(参见图 9~11)消除了裂缝偏向薄弱面的问题,可以使裂缝均匀的生长,降低了井间干扰对于裂缝扩展的影响^[83]。

当井场处于较厚储层或多个储层时,通常需要采用多层立体开发压裂,各产层产生的裂缝应该控制在各自附近位置,防止裂缝窜到相邻产层;可以在满足“W”型布井基础上,压裂中采用交叉的原则,从上到下再从上到下,降低裂缝间互相干扰,提高井网开采效率^[85](见图 12)。美国 QEP 资源开发公司在 Permian 盆地采用多层立体开发,相比于传

统单层开发模式,成本降低 19%^[86]。

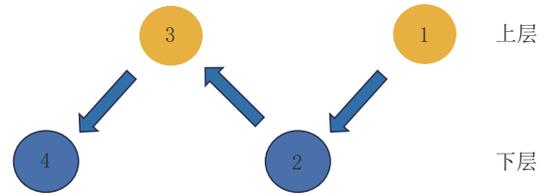


图 12 上、下两层拉链压裂示意

Fig.12 Diagram of zipper fracturing in upper and lower strata

3 发展展望

(1)目前井工厂水力压裂井网布置主要采用丛式水平井布置,其主体思路为:井筒与最小水平主应力平行或小角度相交,使得裂缝近似于垂直井筒,最大可能扩大裂缝接触面积;选取经济合理的水平段长度,增大储层与井筒接触面积;合理布置井筒间距与平台井数,达到既可以充分动用储层又不会产生单井覆盖面积重叠的问题。目前大平台、大井丛已经成为了一种开发趋势。

(2)在水平井多段多簇压裂作业中,宜采用两端长中间短的裂缝长度布置方式。目前的分段分簇原则主要为:单段内岩性、物性、主应力、脆性差异性较小,段内避免对于产层、非产层的同时射孔压裂改造;射孔簇选择以地质甜点为前提,优选段内岩性、地应力一致区域,合理降低裂缝间距使得簇间储层得到充分利用。目前在储层改造过程中单段簇数增多,簇间距缩短,即水平井分段压裂技术整体在合理范围内呈现加密切割储层的趋势。

(3)井工厂水力压裂相对于单口井压裂更加强调施工效率与相邻井筒的裂缝干扰,相比于顺序压裂、交替压裂,拉链压裂工艺可以提供较快施工速度、降低裂缝干扰,更适合井工厂压裂。

(4)针对目前对于井间裂缝扩展应力干扰研究较少;在对于井网设计时,裂缝间距和缝长存在部分简化与近似的问题,建议有针对性的发展立体井网井间裂缝干扰预测、井丛压裂孔簇设计理论。

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